| Tracer | Equation |
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ETD Solver

Numerical Tests

Future Work

Exponential Time Differencing for the Tracer Equations Appearing in Primitive Equation Ocean Models

Sara Calandrini



FLORIDA STATE UNIVERSITY

joint work with Konstantin Pieper and Max Gunzburger

LANL Meeting

January 17, 2019

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| Outline | | | |

- Tracer equation
- ETD solver for the tracer equation
- Numerical tests
- Future Work

| Tracer Equation | ETD Solver | Numerical Tests | Future Work |
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| Tracer Equation & Discretization | | | |

Tracer Equation with vertical discretization

$$\frac{\partial(h_k T_k)}{\partial t} = -\nabla \cdot (h_k u_k T_k) - \overline{T}_k^t w_k^t + \overline{T}_{k+1}^t w_{k+1}^t + [D_h^T]_k + [D_\nu^T]_k ,$$
$$[D_h^T]_k = \nabla \cdot (h_k \kappa_h \nabla T_k) , \quad [D_\nu^T]_k = h_k \delta z_k^m (\kappa_\nu \delta z^t (T_1)) .$$

- *m*, *t*: location as the middle or top of the layer *k* in the vertical
- ":" in subscripts: multiple vertical layers were used for a vertical operator
- κ_h, κ_ν : diffusion

•
$$\overline{\phi}_k^t = \frac{\phi_{k-1} + \phi_k}{2}$$

• $\delta z_k^m(\phi_{:}^t) = \frac{\phi_k^t - \phi_{k+1}^t}{h_k}$
• $\delta z_k^t(\phi_{:}^m) = \frac{\phi_{k-1}^m - \phi_k^m}{(\overline{h})_k^t}$

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| Exact Solution: Exponential Rosenbro | ck Euler method | | |
| Full ETD Solver | | | |

Denote by T the tracer (temperature) and by $T_n \approx T(t_n)$ the current solution at time t_n . Let

$$\partial_t T = F(T) = A_n T + r_n(T)$$
.

This equation is actually linear (u, h and w are constants), so the remainder is zero, namely

$$\partial_t T = F(T) = A_n T$$
.

In this case, we can simply consider the exponential Euler method to find the solution, thus at the time step n + 1

$$T_{n+1} = T_n + \Delta t \varphi_1(\Delta t A_n) F(T_n) .$$

By taking $A_n = F'[T_n]$ (Exponential Rosenbrock Euler), this method gives the exact solution.

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| Operator Splitting | | | |

Splitting Scheme - One stage method

The transport and mixing in the vertical direction cause, in general, more restrictive requirements than the ones for the horizontal. Therefore, the linear operator A_n may be split into

$$A_n = A_n^z + A_n^x \, .$$

Thus,

$$\partial_t T = F(T) = A_n^z T + A_n^x T = A_n^z T + r_n(T) .$$

Using exponential Euler, $r_n(T)$ (= $A_n^{\times}T$) is simply neglected, so the solution is given by

$$T_{n+1} = T_n + \Delta t \varphi_1(\Delta t A_n^z) F(T_n) .$$

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| Operator Splitting | | | |

Splitting Scheme - Two stages method

Using a second stage method following a predictor/corrector approach, we would get

$$T_{n+1}^{1st \, stage} = T_n + \Delta t \varphi_1(\Delta t A_n^z) F(T_n) ,$$

$$T_{n+1} = T_{n+1}^{1st \, stage} + \frac{1}{2} \Delta t \varphi_1(\Delta t A_n^z) (N_{n+1}^{1st \, stage} - N_n) ,$$

where $N_n = F(T_n) - A_n^z T_n$, and $N_{n+1}^{1st \, stage} = F(T_{n+1}^{1st \, stage}) - A_n^z T_{n+1}^{1st \, stage}$, so N takes into account only the contribution from the horizontal terms.

Computationally, to build $N_{n+1}^{1st stage}$ I don't need to construct the full $F(T_{n+1}^{1st stage})$, but only the horizontal terms evaluated at $T_{n+1}^{1st stage}$.

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| Operator Splitting | | | |
| Matrix A_n^z | | | |

Block diagonal structure of A_n^z :



Figure: Simplified case with 4 horizontal elements and 4 vertical layers.

Pros of a block diagonal structure:

- Solving many small problems instead of a large one.
- 2 Easy for parallelization purposes.

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Numerical Tests - Box shape geometry

Velocity Field $(u, w) = (-\psi_1(x)\psi'_2(z), \psi'_1(x)\psi_2(z))$



$$\psi_1(x) = 1 - \frac{\left(x - \frac{x_{max}}{2}\right)^4}{\left(\frac{x_{max}}{2}\right)^4}, \qquad \psi_2(z) = 1 - \frac{\left(z - \frac{z_{min}}{2}\right)^2}{\left(\frac{-z_{min}}{2}\right)^2}$$

with $x_{max} = 10$ and $z_{min} = -10$.

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| Box with a circular velocity field | | | |
| Numerical Tests - | Box shape geor | netry | |

40 layers of height $\Delta z = 0.25$ m $\Delta x = 1$ m so 10 horizontal elements

$$\mathsf{CFL}_x = \frac{\max u \cdot dt}{\Delta x}$$
 and $\mathsf{CFL}_z = \frac{\max w \cdot dt}{\Delta z}$

3 solvers:

- Exponential Rosenbrock Euler (ERE)
- Splitting ETD 2 stages
- RK4 + implicit Euler

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| Box with a circular velocity field | | | |

Numerical Tests - Box shape geometry

ERE (dt = 6): $CFL_z = 19.2$, $CFL_x = 2.4$ Splitting ETD 2 stages (dt = 3): $CFL_z = 9.6$, $CFL_x = 1.2$ RK4 + implicit Euler (dt= 0.5): $CFL_z = 1.6$, $CFL_x = 0.2$

Constant CFL ratio:
$$\frac{CFL_z}{CFL_x} = 8$$

| | $k_ u=2.5\cdot 10^{-5}$ | | |
|------------------------|-------------------------|------------|--------------------|
| | dt | time steps | computational time |
| ERE | 6 | 750 | 16.5680 |
| Splitting ETD 2 stages | 3 | 1500 | 31.8529 |
| RK4 + implicit Euler | 0.5 | 9000 | 89.3249 |

Table: Results for the three solvers, all times are in seconds (s).

Note: n. of vectors in the Krylov basis:

4 vectors for the four central elements and 8 for the six external ones.

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Rectangle with a circular velocity field

Numerical Tests - Rectangle shape geometry

Velocity Field $(u, w) = (-\psi_1(x)\psi'_2(z), \psi'_1(x)\psi_2(z))$



with $x_{max} = 40$ and $z_{min} = -10$.

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| Rectangle with a circular velocity field | | | |

Numerical Tests - Rectangle shape geometry

40 layers of height $\Delta z = 0.25$ m $\Delta x = 1$ m so 40 horizontal elements

CFL ratio: $\frac{CFL_z}{CFL_x} = 8$

| | $k_ u=2.5\cdot 10^{-5}$ | | |
|------------------------|-------------------------|------------|--------------------|
| | dt | time steps | computational time |
| Splitting ETD 2 stages | 2.8 | 5,000 | 244.0533 |
| RK4 + implicit Euler | 0.5 | 28,000 | 669.9195 |

Table: Results for the three solvers, all times are in seconds (s).

Note: n. of vectors in the Krylov basis:

4 vectors for the thirty-four central elements and 8 for the six external ones.

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| Lock Exchange | | | |

Lock Exchange:

Test Description:

- 20 layers, each of which has a thickness of 1 m
- Initial condition for velocity: u = 0 in very layer
- Initial condition for temperature:

$$T(x,z) = \begin{cases} 5, & x < 32 \text{ km}, \\ 30, & x \ge 32 \text{ km}. \end{cases}$$

All diffusion are turned off, so the correct solution is where no mixing occurs, and the front propagates with no intermediate temperatures between 5° C and 30° C. With z-level coordinates, the intermediate layers have temperature

in between 5° C and 30° C.

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| Lock Exchange | | | |

Lock Exchange test case with $\nu_h = 100$:



Figure: (a) our ETD solver, (b) MPAS Ocean.

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| Internal Waves | | | |

Internal Waves:

The initial temperature distribution is $T_0(z) + T'(x, z)$, where

$$T_0(z) = T_{bot} + (T_{top} - T_{bot}) \frac{z_{bot} - z}{z_{bot}}$$
, and

$$T'(x,z) = -A\cos\left(\frac{\pi}{2L}(x-x_0)\right)\sin\left(\pi\frac{z+0.5\Delta z}{z_{bot}+0.5\Delta z}\right),$$

where $T_{bot} = 10.1^{\circ}$ C, $T_{top} = 20.1^{\circ}$ C, $z_{bot} = -487.5$ m, L = 50 km, $x_0 = 125$ km, $x_0 - L < x < x_0 + L$, $\Delta z = 25$ m, and $A = 2^{\circ}$ C.

The perturbation is a single hump of displaced isotherms that initiate symmetric waves propagating out from the center.

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| Internal Waves | | | |

Internal Waves:



Figure: (a) our ETD solver, (b) MPAS Ocean, (c) MITgem , (d) MOM

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| Future Work | | | |
| Future Work | | | |

- Further testing of the splitting ETD scheme with two stages.
- Testing the performances of the proposed solver on more realistic applications.
- Simulating the behavior of multiple tracers in addition to the temperature, such as contaminants and salinity.
- Investigating spatial grid refinements so that passive tracer transport (of, e.g., contaminants) can be handled.

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| References | | | |
| References | | | |

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